

Hoofstuk 3.

Tabel 3-1: Plasmagas-opsies vir gebruik by vergassing.

| Plasma gas | Katodemateriaal | Voordele | Nadele |
|-----------------------|--------------------|--|--|
| Stikstof | Wolfram/Torium | Verlengde katode leeftyd. O ₂ toevoer word afsonderlik beheer. Indien drukwisselabsorpsie (<i>Eng. 'Pressure Swing Absorption' (PSA)</i>) gebruik word, kan die uitskotgas (O ₂) as oksidant gebruik word, afsonderlik beheer en toegevoer. Verminderde NO _x vorming. Optimum katodeleeftyd. | Logistiek (L) geproduseer Verdunning v verbrandings |
| Suurstof | Sirkonium, Hafnium | Goeie beheer oor redokskondisies in die reaktor. Geen verdunning van produkgas met inerte gasse. Lae NO _x . | Logistiek (L) terrein geproc katodeleeftyd |
| Lug | Sirkonium, Hafnium | Eenvoudige logistiek (plaaslike kompressor) | Verdunning v verbrandings Verkorte kato |
| Suurstof-verrykte lug | Sirkonium, Hafnium | Minder verdunning van produkgas met N ₂ as in die geval van lug. Op terrein met drukwisselabsorpsie voorsien. Uitskotgas kan as instrumentlug gebruik word. | Matige verdu verbrandings Verkorte kato |
| CO/CO ₂ | Grafiet | Goedkoop plasmagasse | Nog eksperim |
| Water en/of stoom | | Goedkoop plasmagas, baie hoë entalpie. 100 kW tot 300 kW GS branders kommersieel beskikbaar | Nog nie kom nie |

*[145].

Tabel 3-2: Opsomming van pirometallurgiese aanlegte in Suid-Afrika.

| Produk | Aanlegte | Totale geïnstalleerde vermoë (geraam) | Totale geïnstalleerde kapasiteit |
|---------------------|----------|---------------------------------------|--|
| Aluminium | 2 | Nie beskikbaar | 700 kt a ⁻¹ 175 kt a ⁻¹ (gesluit) |
| Ferrochroom | 14 | 2592 (MVA) | 4240 kt a ⁻¹ |
| Ferromangaan | 4 | Nie beskikbaar | 900 kt a ⁻¹ |
| Ferrosilikon | 3 | Nie beskikbaar | 28 kt a ⁻¹ |
| Ferrovandium | 3 | Nie beskikbaar | 28.25 |
| Kalsiumkarbid | 1 | 52 MVA | 100 kt a ⁻¹ |
| Platinumgroepmetale | 6 | 318 (MVA) | 5.6 M oz a ⁻¹ |
| Silikon | 2 | 48 MVA ~60 MVA | 95 kt a ⁻¹ 55 kt a ⁻¹ (gesluit) |

| | | | |
|----------------|---|----------------|-------------------------|
| Siliko-mangaan | 3 | 193 MVA | 435 kt a ⁻¹ |
| Titaanslak | 3 | 641 MVA | 1528 kt a ⁻¹ |
| Vlekvrystaal | 1 | Nie beskikbaar | Nie beskikbaar |
| Yster en staal | 6 | Nie beskikbaar | 8700 kt a ⁻¹ |

Tabel 3-3: Belangrikste vergassingsreaksies.

| Verbrandingsreaksies | Reaksiewarmte | |
|--|-------------------------------|------------------------------|
| $C + \frac{1}{2} O_2 \rightarrow CO$ | -9.25 MJ/kg -111 MJ/kmol | [1] |
| $CO + \frac{1}{2} O_2 \rightarrow CO_2$ | -10 MJ/kg -283 MJ/kmol | [2] |
| $H_2 + \frac{1}{2} O_2 \rightarrow H_2O$ | -121 MJ/kg -242 MJ/kmol | [3] |
| Heterogenefase reaksies | | |
| $C + H_2O \rightleftharpoons CO + H_2$ | + 10.9 MJ/kg + 131 MJ/kmol | (Watergas reaksie) [4] |
| $C + CO_2 \rightleftharpoons 2 CO$ | + 14.3 MJ/kg + 172 MJ/kmol | (Tru-Boudouard reaksie) [5] |
| $C + 2H_2 \rightleftharpoons CH_4$ | -6.25 MJ/kg -75 MJ/kmol | (Metanering) [6] |
| Verskuiwingsreaksies | | |
| $CO + H_2O \rightleftharpoons CO_2 + H_2$ | -1.46 MJ/kg -41 MJ/kmol | (Water-gas-verskuiwing) [7] |
| $CH_4 + H_2O \rightleftharpoons CO_2 + 3H_2$ | +12.9 MJ/kg + 206 MJ/kmol | (Stoom-metaan-omvorming) [8] |

Tabel 3-4: Voorbeelde van kommersiële vergassers.

| Tipe | Tegnologie/kenmerke | Voermateriaal | Oksidasiegas |
|---------------------------------------|--|------------------|-----------------------|
| GE/ChevronTexaco. | Hoëdruk, enkelstadium, afwaartse sleurvloei, slakvormend, 45 jaar nywerheidsbedryf | Steenkoolflodder | O ₂ |
| CB&I E-gas (ConocoPhilips) | Hoëdruk, twee-stadium, opwaartse sleurvloei, slakvormend. | Steenkoolflodder | O ₂ |
| Shell | Hoëdruk, enkelstadium, afwaartse sleurvloei, slakvormend. | Droë steenkool | O ₂ /stoom |
| Siemens/Babcock Borsig | Hoëdruk, enkelstadium, sleurvloei, slakvormend. | Droë steenkool | O ₂ |

| | | | | |
|--|---|---|-----------------------------------|----|
| Uhde-Prenflow [211] | Hoëdruk, enkelstadium, afwaartse sleurvloei, slakvormend. | Droë steenkool/ petroleumkooks | O ₂ | |
| Siemens | Hoëdruk, sleurvloei, slakvormend | Droë steenkool (antrasiet tot ligniet), ook biomassa, petroleumkooks, afval olie. | O ₂ | |
| Mitsubishi Heavy Industries (MHI) | Hoëdruk, tweestadium, opwaartse sleurvloei, slakvormend | Droë laegraadse steenkool | Lug | |
| ECUST | Hoëdruk, hoëtemperatuur, afwaartse sleurvloei | Steenkoolflodder. Droë steenkoolpoeier met pneumatiese transport (N ₂ of CO ₂) | Lug, O ₂ | |
| Lürgi | Hoëdruk, bewegende bed, droë-as-vergasser, laetemperatuur (<1 000°C), asvormend (SASOL) | Growwe steenkool | Stoom/O ₂ | |
| British Gas Lürgi (BGL) | Hoëtemperatuur, vaste/bewegende bed, slakvormende weergawe van die Lürgi vergasser. | Droë steenkool. Mengsels van hout/ bande/gesorteerde afval kan toegevoeg word. | Stoom/ O ₂ | |
| Kellogg, Brown en Root (KBR) | Tweestadium, hersirkulerende sweefbed, asvormend | Droë, growwe laegraadse steenkool/kalksteen | Stoom/lug stoom/O ₂ | of |
| U-Gas | Enkelstadiumsweefbed | Droë steenkool, petroleumkooks, biomassa, nywerheidsafval en kombinasies daarvan. | Stoom/lug stoom/O ₂ | of |
| Hoëtemperatuur Winkler vergasser | Hoëdruk, hersirkulerende sweefbed, asvormend. | Droë steenkool, biomassa. | Lug of O ₂ | |

Hoofstuk 4.

Tabel 4-1: Gepubliseerde proksimale analises.

| Outeur | Vlugstowwe (massa %) | Vaste koolstof (massa %) | Vog (massa %) | As (massa %) | Staal (massa %) |
|------------------|---------------------------------|-------------------------------------|--------------------------|-------------------------|----------------------------|
| Juma et al | 61.61 | 22.66 | 1.72 | 14.01 | |
| Rodrigues* | 58.8 | 27.7 | | 3.9 | 9.6 |
| Lee | 67.3 | 28.5 | 0.5 | 3.7 | |
| Chang | 62.32 | 26.26 | 1.31 | 10.29 | |
| Gonzales | 61.9 | 29.2 | 0.7 | 8 | |
| Chen** | 93.73 | | 0.54 | 5.3 | |
| Loresgoiti | 59.3 | 27.6 | | 3.5 | 9.6 |
| Orr | 68.7 | 23.3 | 0.4 | 7.6 | |
| Williams | 65.3 | 30.3 | 0.8 | 2.4 | |
| Atal | 58.7 | 33.6 | | 7.7 | |
| Gemiddeld | 65.77 | 27.68 | 0.85 | 6.64 | 9.60 |

| | | | | | |
|-------------------------|-------|------|------|------|------|
| Std afwyking (%) | 10.42 | 3.38 | 0.49 | 3.61 | 0.00 |
|-------------------------|-------|------|------|------|------|

*Staalkoord-versterk; **Gefikseerde C ingesluit.

Tabel 4-2: Gepubliseerde en eie elementanalises.

| Outeur | C (massa %) | H (massa %) | N (massa %) | S (massa %) | O (massa %) | As (massa %) |
|-------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|-------------------------|
| Juma et al | 81.24 | 7.36 | 0.49 | 1.99 | 8.92 | |
| Rodrigues* | 74.2 | 5.8 | 0.3 | 1.5 | 4.7 | 13.5 |
| Lee | 83.8 | 7.6 | 0.4 | 1.4 | 3.1 | 3.7 |
| Chang | 74.4 | 6.96 | 0.21 | 1.6 | 5.02 | 10.21 |
| Gonzales | 86.7 | 8.1 | 0.4 | 1.4 | 1.3 | 2.9 |
| Chen** | 81.16 | 7.22 | 0.47 | 1.64 | 2.07 | 7.44 |
| Berruoco | 88.5 | 6.6 | 0.4 | 1.6 | 3 | |
| Arion | 73.8 | 5.3 | 0.44 | 1.71 | 0.11 | 17.8 |
| Loresgoiti | 74.2 | 5.8 | 0.3 | 1.5 | 5.1 | 13.1 |
| Orr | 81.3 | 7.3 | 0.3 | 1.5 | | 1.4 |
| Williams | 85.8 | 8 | 0.4 | 1 | 2.3 | 2.4 |
| Lanoir | 82.63 | 7.5 | 0.36 | 1.69 | | |
| Senneca | 86.7 | 6.9 | 0.3 | 1.9 | 1 | 3.3 |
| Roy | 86.6 | 8.1 | 0.5 | 0.8 | 2.2 | |
| Cunliffe | 86.4 | 8 | 0.5 | 1.7 | 3.4 | 2.4 |
| Mediaan | 81.20 | 7.09 | 0.40 | 1.55 | 3.10 | 8.83 |
| Gemiddelde | 79.93 | 6.80 | 0.37 | 1.58 | 3.70 | 8.76 |
| Std afwyking | 5.51 | 0.91 | 0.09 | 0.17 | 2.60 | 5.87 |
| Necsa* (2016) | 83.72 | 6.58 | 0.68 | 0.34 | 6.14 | 2.23 |
| Hierdie studie** | 82.97 | 7.06 | 0.04 | 1.33 | 1.16 | 7.44 |
| Verskil (%) | 2.52 | -0.51 | 0.28 | -1.21 | 3.04 | -6.60 |

* Tekstiel-versterk; ** Industriële monster SRC1-5, gebruik vir stoigiometrie-berekeninge.

Tabel 4-3: Gepubliseerde pirolise-entalpiewaardes vir rubber.

| Outeur | ΔH° (kJ kg⁻¹) |
|----------------------------|---|
| Bekkedahl & Matheson [223] | 507 ±100 |
| Lanteigne et al. [224] | 550 |
| Yang & Roy [225] | 560 |
| Gemiddelde | 539±27 |

Hoofstuk 5.

abel 5-1: Kinetiese modelle vir vastetoestandreaksies.

| | Reaksiemodel | Kode | $f(\alpha)$ | $g(\alpha)$ |
|----|---|------|--|--|
| 1 | Magswet | P4 | $4\alpha^{3/4}$ | $\alpha^{1/4}$ |
| 2 | Magswet | P3 | $3\alpha^{2/3}$ | $\alpha^{1/3}$ |
| 3 | Magswet | P2 | $2\alpha^{1/2}$ | $\alpha^{1/2}$ |
| 4 | Magswet | P2/3 | $(2/3)\alpha^{-1/2}$ | $\alpha^{3/2}$ |
| 5 | Mampel (eerste-orde) | F1 | $1 - \alpha$ | $-\ln(1 - \alpha)$ |
| 6 | Avrami-Erofeev | A4 | $4(1 - \alpha)[-\ln(1 - \alpha)]^{3/4}$ | $[-\ln(1 - \alpha)]^{1/4}$ |
| 7 | Avrami-Erofeev | A3 | $3(1 - \alpha)[-\ln(1 - \alpha)]^{2/3}$ | $[-\ln(1 - \alpha)]^{1/3}$ |
| 8 | Avrami-Erofeev | A2 | $2(1 - \alpha)[-\ln(1 - \alpha)]^{1/2}$ | $[-\ln(1 - \alpha)]^{1/2}$ |
| 9 | Krimpde sfeer | R3 | $3(1 - \alpha)^{2/3}$ | $1 - (1 - \alpha)^{1/3}$ |
| 10 | Krimpde silinder | R2 | $2(1 - \alpha)^{1/2}$ | $1 - (1 - \alpha)^{1/2}$ |
| 11 | Eendimensionele diffusie | D1 | $(1/2)\alpha^{-1}$ | α^2 |
| 12 | Tweedimensionele diffusie | D2 | $[-\ln(1 - \alpha)]^{-1}$ | $(1 - \alpha)\ln(1 - \alpha) + \alpha$ |
| 13 | Driedimensionele diffusie (Jander) | D3 | $(3/2)(1 - \alpha)^{2/3}[1 - (1 - \alpha)^{1/3}]^{-1}$ | $[1 - (1 - \alpha)^{1/3}]^2$ |
| 14 | Driedimensionele diffusie (Ginstling-Brounshtein) | D4 | $(3/2)[(1 - \alpha)^{-1/3} - 1]^{-1}$ | $1 - (2/3)\alpha - (1 - \alpha)^{2/3}$ |

Tabel 5-2: Kinetiese modelle gebruik vir gas-vastetoestandreaksies.

| | Reaksiemodel | Kode | $d\alpha/dt = f(\alpha)/\tau$ | $g(\alpha) = t/\tau$ | τ |
|---|--|------|---|---|---------------------------------------|
| 1 | Gasfilmdiffusiebeheer | L1 | 1 | α | $\frac{\rho_B R}{3bk_g C_{Ag}}$ |
| 2 | Aslaagdiffusiebeheer | L2 | $[2(1 - \alpha)^{-1/3} - (1 - \alpha)^{-1}]^{-1}$ | $1 - 3(1 - \alpha)^{2/3} + 2(1 - \alpha)$ | $\frac{\rho_B R^2}{6bDk_{eg} C_{Ag}}$ |
| 3 | Krimpde sfeer met chemiese reaksiebeheer | L3 | $3(1 - \alpha)^{2/3}$ | $1 - (1 - \alpha)^{1/3}$ | $\frac{\rho_B R}{bk'' C_{Ag}}$ |

Notas: Levenspiel se simbole word gebruik. R is die radius van die vastestofpartikel, ρ_B is die digtheid daarvan, C_{Ag} is die konsentrasie van die reagerende gas en b is die stoigiometriesse koëffisient vir die reaksie, genormaliseer t.o.v. die vastestof, d.i. $\text{Fluïede} + b\text{Vastestof} \rightarrow \text{Produkte}$. k_g en k'' is die tempokonstantes en D_e is die diffusiekoëffisient van die produkte deur die aslaag

Tabel 5-3: ANOVA-analise vir die modelkeuses vanaf isotermiese data.

| Pirolise <550 °C | Pirolise >550 °C | Tru-Boudouard |
|------------------|------------------|---------------|
|------------------|------------------|---------------|

| Model | Aantal T's | Gem R ² | Var | Aantal T's | Gem R ² | Var | Model | Aantal T's | Gem R ² | Var |
|---------|---------------|--------------------|--------|---------------|--------------------|--------|--------|---------------|--------------------|--------|
| P4 | 4 | 0.8956 | 0.0051 | 6 | 0.9741 | 0.0004 | L1 | 6 | 0.9123 | 0.0317 |
| P3 | 4 | 0.9015 | 0.0047 | 6 | 0.9763 | 0.0004 | L2 | 6 | 0.9894 | 0.0004 |
| P2 | 4 | 0.9126 | 0.0041 | 6 | 0.9801 | 0.0004 | L3 | 6 | 0.9949 | 0.0001 |
| P2/3 | 4 | 0.9624 | 0.0013 | 6 | 0.9899 | 0.0002 | | | | |
| F1 | 4 | 0.9593 | 0.0008 | 6 | 0.9931 | 0.0001 | | | | |
| A4 | 4 | 0.9124 | 0.0024 | 6 | 0.9845 | 0.0002 | | | | |
| A3 | 4 | 0.9188 | 0.0021 | 6 | 0.9864 | 0.0002 | | | | |
| A2 | 4 | 0.9306 | 0.0017 | 6 | 0.9895 | 0.0001 | | | | |
| R3 | 4 | 0.9539 | 0.0011 | 6 | 0.9926 | 0.0001 | | | | |
| R2 | 4 | 0.9509 | 0.0013 | 6 | 0.9919 | 0.0001 | | | | |
| D1 | 4 | 0.9767 | 0.0006 | 6 | 0.9875 | 0.0001 | | | | |
| D2 | 4 | 0.9817 | 0.0003 | 6 | 0.9868 | 0.0001 | | | | |
| D3 | 4 | 0.9860 | 0.0001 | 6 | 0.9835 | 0.0001 | | | | |
| D4 | 4 | 0.9833 | 0.0002 | 6 | 0.9860 | 0.0001 | | | | |
| F: | | | 2.2450 | | | | 1.1262 | | | 1.1900 |
| F crit: | | | 1.9612 | | | | 0.3527 | | | 3.6823 |
| P: | | | 0.0241 | | | | 1.8627 | | | 0.3314 |

Tabel 5-4: Afgeleide isothermiese kinetiese parameters.

| | Pirolise stap 1 | | Pirolise stap 2 | | Tru-Boudouard | |
|--------------------------------|---------------------|------------------------|------------------------|------------------------|---------------------|------------------------|
| Model: | D3 | | F1 | | L3 | |
| Temperatuurbereik | 200–550 °C | | 550–1 000 °C | | 750–1 100 °C | |
| | Aanvanklik | Verfyn | Aanvanklik | Verfyn | Aanvanklik | Verfyn |
| q : | 1 | 0 | 1 | 5.0×10^{-2} | 1 | 5.664×10^{-3} |
| k_0 (min ⁻¹): | 4.006×10^6 | 7.337×10^8 | 1.286×10^{-1} | 6.647×10^{-2} | 4.232×10^7 | 2.580×10^6 |
| r : | 1 | 2.578×10^{-2} | 1 | 1.0×10^{-2} | 1 | 0 |
| E_A (kJ mol ⁻¹): | 111.6 | 140.0 | 35.7 | 35.7 | 232.21 | 168.9 |

Tabel 5-5: Afgeleide parameters vir die Sestak-Berggren-modelle.

| S-B parameter | N ₂ stap 1 | N ₂ stap 2 | CO ₂ stap 1 | CO ₂ stap 2 |
|-------------------------------|------------------------|------------------------|------------------------|------------------------|
| m | 0 ⁵ | 2.000×10^{-1} | 3.335×10^{-2} | 0 |
| n | 2.196 | 0 | 1.871 | 1.133×10^{-2} |
| p | 7.410×10^{-5} | 6.519×10^{-2} | 2.146×10^{-5} | 1.959×10^{-8} |
| q | 0 | 0 | 0 | 5.930×10^{-2} |
| r | 0 | 6.500×10^{-1} | 7.952×10^{-4} | 0 |
| k_0 (min ⁻¹) | 4.391×10^8 | 6.775×10^{-3} | 3.882×10^7 | 1.751×10^4 |
| E_A (kJ mol ⁻¹) | 117.0 | 105.0 | 103.7 | 110.3 |

Tabel 5-6: Gemiddelde absolute foute tussen eksperimentele waardes en modelsimulasies vir dinamiese termogramme.

| Reaksie | Isotermies | Sestak-Berggren |
|--|------------|-----------------|
| N ₂ pirolise 200–550 °C | 2.1 % | 3.4 % |
| N ₂ pirolise 550–1 000 °C | 1.6 % | 2.5 % |
| CO ₂ pirolise 200–550 °C | 2.0 % | 3.6 % |
| CO ₂ tru-Boudouard 750–1 100 °C | 0.5 % | 1.1 % |

Tabel 5-7: Vergelyking van kinetiese data vir die tru-Boudouardreaksie.

| Outeurs | Materiaal | TGA regime | Model | E_A (kJ mol ⁻¹) | P_{CO_2} (atm) | Verwysing |
|---------------|--------------------|------------|---|----------------------------------|---------------------|-----------|
| Dutta e.a. | Steenkool kooks | Isotermies | Reaksiebeheer met intrapartikel diffusie | 248 | 1 | [257] |
| Lee en Kim | Bandekooks | Isotermies | *MVRM | 238.9 | 0.3–1.0 | [258] |
| Issac e.a. | Bandekooks | Isotermies | *RPM | 174.9–177.0 | 1 | [246] |
| Murillo e.a. | Bandekooks | Isotermies | *VM, MVM, CGSM, RPM | 191.4–197.7 | 0.2–0.4 | [259] |
| Betancur e.a. | Bandekooks | Isotermies | *CGSM, RPM, HMRPM | 147.3–155.5 | 0.2–0.3 | [260] |
| Hierdie werk | Bandekooks | Isotermies | *L3 | 201.7–223.1 | 1.0 | |

*MVRM - 'Modified Volume Reaction Model'; RPM - 'Random Pore Model'; VM - 'Volume reaction Model'; MVM - 'Modified Volume reaction Model'; CGSM - 'Changing Grain Size Model'; HMRPM - 'Hybrid Modified Random Pore Model'; L3 – Krimpde-sfeer reaksiebeheermodel.

Hoofstuk 6.

Tabel 6-1: Rubbereienskappe.

| Komponent | Massa % |
|----------------------|---------|
| Gefikseerde koolstof | 19.04 |
| Vlugstowwe | 70.81 |
| As | 10.15 |
| C | 74.495 |
| H | 6.556 |
| N | 0.025 |
| S | 2.196 |
| O (deur verskil) | 6.575 |

Tabel 6-2: Opsomming van eksperimentele kondisies.

| Eksp. no | Prosesgas | Blokkie nom. wand lengte | Blokkie nom. volume | Blokkie ware volume | Aanvangs- massa | T | Tyd |
|----------|-----------------|--------------------------------|---------------------------|---------------------------|--------------------|------|-------|
| | | (mm) | (cm ³) | (cm ³) | (g) | (°C) | (min) |
| 220329_2 | CO ₂ | 5 | 0.125 | 0.147 | 0.1676 | 863 | 23 |
| 220224_1 | N ₂ | 10 | 1.00 | 0.965 | 1.0989 | 635 | 22 |
| 220324_3 | CO ₂ | 10 | 1.00 | 1.204 | 1.3710 | 863 | 20 |
| 220329_1 | CO ₂ | 15 | 3.375 | 3.199 | 3.6440 | 456 | 21 |
| 220302_1 | N ₂ | 15 | 3.38 | 3.2836 | 2.843 | 640 | 22 |
| 220302_2 | CO ₂ | 15 | 3.375 | 3.493 | 3.9789 | 640 | 20 |
| 220310_1 | CO ₂ | 15 | 3.375 | 2.508 | 2.8566 | 873 | 10 |
| 220322_1 | CO ₂ | 15 | 3.375 | 3.252 | 3.7040 | 864 | 14 |
| 220310_2 | CO ₂ | 15 | 3.38 | 3.116 | 3.5488 | 882 | 20 |
| 220318_1 | CO ₂ | 15 | 3.38 | 3.178 | 3.6196 | 860 | 20 |
| 220316_1 | CO ₂ | 15 | 3.38 | 2.540 | 2.8935 | 861 | 45 |
| 220324_1 | CO ₂ | 15 | 3.38 | 3.363 | 3.8303 | 862 | 20 |
| 220505_1 | CO ₂ | 15 | 3.38 | 3.712 | 4.2275 | 990 | 20 |
| 220328_1 | CO ₂ | 20 | 8.00 | 8.112 | 9.2394 | 864 | 23 |

Die massaverskille tussen nominaal ewe groot blokkies kan toegeskryf word aan hoe moeilik dit is om die monsters akkuraat met die hand te sny.

Tabel 6-3: Vergelykende fisiese eienskappe.

| Materiaal | a_T (mm ² s ⁻¹) | α (W/(m K)) | C_p J/(kg K) | ρ (kg m ⁻³) |
|-----------------------------------|---|-----------------------|-------------------|---------------------------------|
| Hierdie ondersoek | 0.194 | - | - | - |
| *Butadien-akrilonitrielerubber +C | 0.22 | 0.418 | 1443 | 1 340 |
| *Stireen-butadienrubber + CB | 0.14 | 0.243 | 1757 | 1 000 |
| **Bandrubber | 0.281 | 0.38 | 1230 | 1 100 |

*Thermtest databasis [281], ** Yang e.a. [54].

Tabel 6-4: Opsomming van termiese diffusiwiteite en $D = 0$ pirolisetyd afsnitte.

| T (°C) | $\tau_{0,model}$ (s) | $\tau_{0,eksperimenteel}$ (s) | α_T (mm ² s ⁻¹) | Verwysing |
|-------------|-------------------------|----------------------------------|--|--------------|
| 490 | 312.9 | 256.8 | 0.126 | [277] |
| 501 | 228.7 | 93.8 | 0.161 | [43] |
| 544 | 72.8 | 25.1 | 0.147 | [43] |
| 550 | 62.7 | 70.1 | 0.149 | [270] |
| 590 | 24.3 | 9.5 | 0.173 | [43] |
| 620 | 12.6 | 110.5 | 0.178 | [277] |
| 840 | 0.3 | 17.8 | 0.209 | [277] |
| 860 | 0.2 | 0 | 0.194 | Hierdie werk |
| Gemiddeld: | | | 0.166 ±0.026 | |

Tabel 6-5: Opgesomde kinetiese data vir pirolise en die tru-Boudouardreaksie in integrale vorm as $g(\alpha) = \frac{t}{\tau}$.

| $g(\alpha)$ | τ (min) | Verg. no |
|--|---|--|
| Pirolise | | |
| $[1 - (1 - \alpha)^{1/3}]^2$ | $\left[k_0 e^{-\frac{E_a}{RT}} \right]^{-1}$ | $k_0 = 7.337 \times 10^8 \text{ min}^{-1}$ $E_a = 1.40 \times 10^5 \text{ J mol}^{-1} \text{ K}^{-1}$ (6-1) |
| Tru-Boudouard – chemiese reaksie beheer | | |
| $1 - (1 - \alpha)^{1/3}$ | $\left[\frac{k_0 e^{-\frac{E_a}{RT}} C_{CO_2}}{\rho_C R_0} \right]^{-1}$ | $k_0 = 2.58 \times 10^6 \text{ m min}^{-1}$ $E_a = 1.69 \times 10^5 \text{ J mol}^{-1} \text{ K}^{-1}$ (6-2) |
| Tru-Boudouard – massa-oordrag beheer | | |
| $1 - (1 - \alpha)^{2/3}$ | $\left[\frac{Sh D_{CO_2} C_{CO_2}}{\rho_C R_0^2} \right]^{-1}$ | $Sh = 2 + 0.522 Re^{1/2} Sc^{1/3}$ $Re = \frac{\rho_{CO_2} u_{CO_2} R_0}{\mu_{CO_2}}$ (6-3) |

$$Sc = \frac{\mu_{CO_2}}{\rho_{CO_2} D_{CO_2}}$$

Hier is: C_{CO_2} die parsieële druk van die CO₂, uitgedruk as massa per; ρ die digtheid met die onderskrif wat óf C óf CO₂ aandui; D_{CO_2} die self-diffusiekonstante van CO₂; Sh die Sherwoodgetal; Re die Reynoldsgetal; Sc die Schmidtgetal; en μ_{CO_2} die CO₂ viskositeit.

Hoofstuk 7.

Tabel 7-1: Hoopdigthede van rubbermonsters.

| Monster | Los hoopdigtheid (kg/m ³) | Gepakte hoopdigtheid (kg/m ³) |
|------------------|---------------------------------------|---|
| < 1 mm skaafsels | 288.5 | 361.1 |
| 3–5 mm korrels | 481.5 | 515 |
| 6–12 mm snippers | 485.7 | 485.7 |

Tabel 7-2: Opsomming van plasma-eksperimente uitgevoer.

| Eksp. no | Partikelgrootte (mm) | Voer (kg/h) | N ₂ (kg/h) | CO ₂ (kg/h) | Plasma (kW _(e)) | Reaktor (°C)(min) | Reaktor (°C)(maks) |
|-------------------------|----------------------|-------------|-----------------------|------------------------|-----------------------------|-------------------|--------------------|
| Inbedryfstelling | | | | | | | |
| 220908_1 | | | 2.54 | 4.6 | 12 | 865 | 898 |
| 220913_1 | | | 2.54 | 1.36 | 12.87 | 990 | 1017 |
| 220915_1 | <1 | 0.5 | 2.04 | 1.9 | 16.7 | 965 | 1037 |
| 220922_1 | <1 | 0.75 | 2.42 | 1.9 | 14.72–15.8 | | 1057 |
| Eksperimente | | | | | | | |
| 220928_1 | <1 | 1 | 2.42 | 1.9 | 15.6 | 845 | 1026 |
| | | 1.5 | 2.42 | 1.9 | 15.6 | 837 | 1023 |
| 221005_1 | <1 | 0.5 | 2.42 | 1.9 | 15.84 | 994 | 1235 |
| | | 0.75 | 2.42 | 1.9 | 15.18 | 1160 | 1203 |
| 221020_1* | 3–5 | 0.5 | 2.42 | 0 | 15 | 947 | 1246 |
| | 3–5 | 0.75 | | | | 846 | 1441 |
| | 3–5 | 1 | | | | 1394 | 1574 |
| 221102_1 | 3–5 | 1.73 | 2.42 | 1.9 | 16.6 | 981 | 1163 |
| 221123_1 | 3–5 | 1.73 | 2.42 | 1.9 | 16.56 | 970 | 1157 |
| 221207_1 | 6–12 | | 2.42 | 1.9 | | 1985 | 1192 |

*Lopie na 50 min gestaak om toerusting te beskerm teen oorverhitting; **4 kg h⁻¹ (nom), lopie moes na 45 min gestaak word weens voerfaling.

Tabel 7-3: Reaktorvertoef tyd en partikel uitsaksnelheid

| Rubber voertempo | 0.5 kg h ⁻¹ | 0.161 cm ³ g ⁻¹ | | |
|--------------------------|--|---------------------------------------|--|---|
| Reaktor binmedia: | 0.2 m | Diepte | 0.15 m | |
| Buitedia | 0.24 m | Hoogte | 0.18 m | |
| Gasvertoeflyd berekening | | | Uitsaksnelheid berekeningparameters | |
| Reaktorvolume | 4.71×10 ⁻³ m ³ | | Temperatuur | T 1273 K |
| Reaktor area | 3.14×10 ⁻² m ² | | Partikel digtheid** | ρ _p 700 kg m ⁻³ |
| Temp | 1 000 C | | Gasdigtheid | ρ 0.277 kg m ⁻³ |
| | 1273 K | | Swaartekragversnelling | g 9.8 m s ⁻² |
| N ₂ vloe | 2.9×10 ⁻³ m ³ s ⁻¹ | 10.26 m ³ h ⁻¹ | Partikeldiameter | d 1×10 ⁻⁴ m |
| Ar vloe | 4.32×10 ⁻⁴ m ³ s ⁻¹ | 1.56 m ³ h ⁻¹ | Kinetiese viskositeit (lug, N ₂) | μ 1.71×10 ⁻⁴ m ² s ⁻¹ |
| CO ₂ vloe | 1.42×10 ⁻³ m ³ s ⁻¹ | 5.1 m ³ h ⁻¹ | | |
| Produkte | 6.12×10 ⁻⁴ m ³ s ⁻¹ | 2.2 m ³ h ⁻¹ | | |
| Totaal | 4.7×10 ⁻³ m ³ s ⁻¹ | 16.91 m ³ h ⁻¹ | | |
| Maks. Vertoeflyd | 1.00 s | | Uitsaksnelheid | |
| Min. Gassnelheid | 0.15 m s ⁻¹ | | Yalin (> 2 mm) | (ρ _p -ρ _m)gd ³ /ρ _m μ ² 9.92×10 ⁻¹ m s ⁻¹ |
| | | | Stokes (< 2 mm) | 2/9(ρ _p -ρ _m)gd ² /μ 8.89×10 ⁻² m s ⁻¹ |

* Eksp 220928; ** [292, 293]

Tabel 7-4: Gasdigthede

| | kg m ⁻³ (NTD*) | kg m ⁻³ (STD**) |
|--------------------------|---------------------------|----------------------------|
| Lug | 1.205 | 1.029 |
| N ₂ | 1.165 | 1.251 |
| O ₂ | 1.331 | 1.429 |
| H ₂ O(g) | 0.804 | — |
| H ₂ | 0.08375 | 0.0899 |
| Sintese gas [#] | 0.569 | 0.622 |

*(20°C, 101.3 kPa) ** (0 °C, 101.3 kPa); # Bereken vanaf verg. (7-1).

Die digtheid van die sintese gas in Tabel 7-4 is bereken uit

$$\rho_g = \frac{pM_g}{RT} \quad (7-1)$$

Tabel 7-5: Sintese gas-samestelling en berekende opbrengste, <1 mm skaafels.

| | | | | | | | | |
|----------------------|-------------------|--------------|------------|--------------|------------|--------------|------------|--------------|
| Eksp 220915_1 | t = 0: begin voer | | | | | | | |
| Analise no | 1 | | 2 | | 3 | | 4 | |
| Looptyd (min) | 0.17 | | 1 | | 25 | | 33 | |
| Samestelling | mol | % m/m | mol | % m/m | mol | % m/m | mol | % m/m |

| | | | | | | | | |
|--|-------|-------------|------|-------------|------|-------------|------|-------------|
| Totale C | 0.532 | 31% | 0.57 | 32% | 0.50 | 29% | 0.30 | 14% |
| Totale H | 1.167 | 6% | 1.22 | 6% | 0.94 | 5% | 0.00 | 0% |
| Totale O | 0.338 | 27% | 0.35 | 26% | 0.36 | 27% | 0.57 | 36% |
| Totale N | 0.341 | 24% | 0.36 | 24% | 0.38 | 26% | 0.60 | 33% |
| Totale Ar | 0.064 | 13% | 0.06 | 12% | 0.07 | 13% | 0.10 | 16% |
| Totaal | | 100% | | 100% | | 100% | | 100% |
| Ar + N ₂ (kg h ⁻¹) | | 2.36 | | 2.67 | | 2.67 | | 2.67 |
| Singas (kg h ⁻¹) | | 4.17 | | 4.87 | | 4.19 | | 2.69 |
| Singas H _c (MJ kg ⁻¹) | | | | | | | | |
| Afgas (kg h ⁻¹) | | 6.53 | | 7.53 | | 6.86 | | 5.36 |
| Afgas H _c (MJ kg ⁻¹) | | -3.91 | | -4.04 | | -3.50 | | -0.22 |

Tabel 7-6: Sintesegas-samestelling en berekende opbrengste, <1 mm skaafsels.

| | | | | | | |
|--|-------------------|----------------|------------|----------------|------------|----------------|
| Eksp 220922_1 | t = 0: begin voer | | | | | |
| Analise no | 1 | | 2 | | 3 | |
| Looptyd (min) | 1 | | 16 | | 43 | |
| Samestelling | Mol | % m/m | Mol | % m/m | Mol | % m/m |
| Totale C | 0.016 | 0.67% | 0.34 | 13.53% | 0.48 | 22.45% |
| Totale H | 0.054 | 0.19% | 0.21 | 0.69% | 0.84 | 3.30% |
| Totale O | 0.004 | 0.23% | 0.47 | 24.78% | 0.36 | 22.39% |
| Totale N ₂ | 0.780 | 75.88% | 0.57 | 52.32% | 0.41 | 44.23% |
| Totale Ar | 0.166 | 23.03% | 0.07 | 8.67% | 0.05 | 7.63% |
| Totaal | | 100.00% | | 100.00% | | 100.00% |
| Ar + N ₂ (kg h ⁻¹) | | 2.93 | | 2.93 | | 2.93 |
| Singas (kg h ⁻¹) | | 0.03 | | 1.88 | | 2.72 |
| Singas H _c (MJ kg ⁻¹) | | | | | | |
| Afgas (kg h⁻¹) | | 2.97 | | 4.81 | | 5.66 |
| Afgas H _c (MJ kg ⁻¹) | | -0.37 | | -1.67 | | -3.42 |

Tabel 7-7: Sintesegas-samestelling en berekende opbrengste, <1 mm skaafsels.

| Eksp 220928_1 | t = 0: begin voer | | | | | | | |
|--|-------------------|--------------|----------------|--------------|----------------|--------------|----------------|--------------|
| Analise no | 1 | | 2 | | 3 | | 4 | |
| Looptyd (min) | 0 | | 71 | | 95 | | 105 | |
| Samestelling | Mol | % m/m | Mol | % m/m | Mol | % m/m | Mol | % m/m |
| Totale C | 0.43 | 19.22% | 0.22 | 8.31% | 0.03 | 0.68% | 0.201 | 7.55% |
| Totale H | 0.69 | 2.58% | 0.22 | 0.70% | 0.10 | 0.20% | 0.002 | 0.01% |
| Totale O | 0.39 | 23.24% | 0.40 | 19.65% | 0.00 | 0.03% | 0.365 | 18.26% |
| Totale N ₂ | 0.45 | 47.07% | 0.67 | 58.57% | 1.60 | 85.43% | 1.366 | 59.82% |
| Totale Ar | 0.05 | 7.89% | 0.10 | 12.76% | 0.18 | 13.66% | 0.115 | 14.36% |
| Totaal | 100.00% | | 100.00% | | 100.00% | | 100.00% | |
| Ar + N ₂ ((kg h ⁻¹)) | 2.93 | | 2.93 | | 2.93 | | 2.93 | |
| Singas (kg h ⁻¹) | 2.41 | | 1.18 | | 0.03 | | 1.02 | |
| Singas H _c (MJ kg ⁻¹) | | | | | | | | |
| Afgas (kg h ⁻¹) | 5.34 | | 4.11 | | 2.96 | | 3.96 | |
| Afgas H _c (MJ kg ⁻¹) | -2.91 | | -0.41 | | -0.72 | | -0.31 | |

Tabel 7-8: Sintesegas-samestelling en berekende opbrengste, <1 mm skaafsels.

| Eksp 221005_1 | t = 0: begin voer | | | | | | | | | |
|--|-------------------|--------------|----------------|--------------|----------------|--------------|----------------|--------------|----------------|--------------|
| Analise no | 1 | | 2 | | 3 | | 4 | | 5 | |
| Looptyd (min) | 6 | | 21 | | 50 | | 65 | | 80 | |
| Samestelling | Mol | % m/m | Mol | % m/m | Mol | % m/m | Mol | % m/m | Mol | % m/m |
| Totale C | 0.01 | 0.50% | 0.29 | 15.61% | 0.28 | 14.13% | 0.27 | 13.57% | 0.3 | 14.05% |
| Totale H | 0.02 | 0.06% | 0.34 | 1.55% | 0.00 | 0.00% | 0.00 | 0.00% | 0.0 | 0.11% |
| Totale O | 0.01 | 0.45% | 0.41 | 29.45% | 0.52 | 34.92% | 0.50 | 33.88% | 0.5 | 33.90% |
| Totale N ₂ | 1.66 | 77.85% | 0.63 | 39.11% | 0.64 | 37.11% | 0.64 | 37.78% | 0.6 | 37.77% |
| Totale Ar | 0.16 | 21.13% | 0.08 | 14.28% | 0.08 | 13.84% | 0.09 | 14.77% | 0.1 | 14.17% |
| Totaal | 100.00% | | 100.00% | | 100.00% | | 100.00% | | 100.00% | |
| Ar + N ₂ (kg h ⁻¹) | 2.73 | | 2.73 | | 2.73 | | 2.73 | | 2.73 | |
| Singas (kg h ⁻¹) | 0.03 | | 2.39 | | 2.63 | | 2.47 | | 2.53 | |
| Singas H _c (MJ kg ⁻¹) | | | | | | | | | | |
| Afgas (kg h ⁻¹) | 2.76 | | 5.12 | | 5.37 | | 5.20 | | 5.26 | |
| Afgas H _c (MJ kg ⁻¹) | -0.25 | | -1.39 | | -0.33 | | -0.27 | | -0.28 | |

Tabel 7-9: Oppervlak-analise van koolresidu uit tru-Boudouard vergassing

| Oppervlakarea (m² g⁻¹) | Duplikaatwaardes | |
|---|-------------------------|-------|
| Enkelpunt oppv. area by p/p° = 0.30 | 54.88 | 46.02 |
| BET oppv. area | 56.74 | 47.91 |
| t-Stipping eksterne oppv. area | 62.11 | 56.62 |
| BJH Adsorpsie kumulatiewe oppv. area porieë 17 000 Å en 3 000 000 Å wyd | 57.9 | 53.09 |
| BJH Desorpsie kumulatiewe oppv. area porieë 17 000 Å en 3 000 000 Å wyd | 59.89 | 55.69 |

| Porievolume (cm³ g⁻¹) | | |
|---|---------|---------|
| Enkelpunt adsorpsie: totale porievolume: porië <777.963 Å wyd by p/p° = 0.97 | 0.169 | 0.18 |
| Enkelpunt desorpsie totale porievolume: porië <19.64 Å wyd by p/p° = 0.15 | 0.022 | 0.018 |
| t-Stipping mikroporie volume | -0.0029 | -0.0047 |
| BJH Adsorpsie kumulatieve volume, porië tussen 17 000 Å en 3 000 000 Å width | 0.27 | 0.27 |
| BJH Desorption cumulative volume of pores between 17 000 Å en 3 000 000 Å wyd | 0.26 | 0,27 |
| Poriegrootte (Å) | | |
| Adsorpsie gem. poriediameter (4V/A m.b.v. BET) | 113.44 | 146.13 |
| Desorpsie gem. poriediameter (4V/A m.b.v. BET) | 15.17 | 14.76 |
| BJH Adsorpsie gem. poriewydte (4V/A) | 183.28 | 204.60 |
| BJH Desorpsie gem. poriewydte (4V/A) | 176.32 | 194.60 |

Tabel 7-10: Sintesegas samestelling en berekende opbrengste, 35 mm krummels

| Eksp 221020_1 | | | | | | | | | | | | | | |
|---|------------|--------------|------------|--------------|------------|--------------|------------|--------------|------------|--------------|------------|--------------|------------|--------------|
| Analises | 1 | | 2 | | 3 | | 4 | | 5 | | 6 | | 7 | |
| t = 0: plasma aan | 10:32:00 | | 10:41:20 | | 10:55:10 | | 11:04:00 | | 11:17:00 | | 11:25:50 | | 11:38:00 | |
| Looptyd (min) | 26 | | 35 | | 49 | | 58 | | 71 | | 80 | | 85 | |
| Samestelling | Mol | % m/m | Mol | % m/m | Mol | % m/m | Mol | % m/m | Mol | % m/m | Mol | % m/m | Mol | % m/m |
| Totale C | 0.00 | 0.05% | 0.00 | 0.12% | 0.00 | 0.15% | 0.00 | 0.11% | 0.00 | 0.15% | 0.00 | 0.02% | 0.00 | 0.14% |
| Totale H | 0.00 | 0.00% | 0.00 | 0.00% | 0.00 | 0.00% | 0.00 | 0.00% | 0.00 | 0.01% | 0.00 | 0.00% | 0.00 | 0.00% |
| Totale O | 0.00 | 0.14% | 0.01 | 0.31% | 0.01 | 0.39% | 0.01 | 0.29% | 0.01 | 0.41% | 0.00 | 0.05% | 0.01 | 0.38% |
| Totale N ₂ | 1.63 | 75.70% | 1.63 | 75.85% | 1.63 | 75.84% | 1.64 | 76.12% | 1.64 | 76.19% | 1.63 | 75.82% | 1.64 | 77.15% |
| Totale Ar | 0.18 | 24.11% | 0.18 | 23.73% | 0.18 | 23.62% | 0.18 | 23.49% | 0.18 | 23.24% | 0.18 | 24.11% | 0.17 | 22.33% |
| Totaal | 100.00% | | 100.00% | | 100.00% | | 100.00% | | 100.00% | | 100.00% | | 100.00% | |
| N ₂ + Ar (kg/h) | 2.93 | | 2.93 | | 2.93 | | 2.93 | | 2.93 | | 2.93 | | 2.93 | |
| Singas (kg/h) | 0.0057 | | 0.0125 | | 0.0160 | | 0.0118 | | 0.0168 | | 0.0021 | | 0.0153 | |
| Afgas (kg/h) | 2.94 | | 2.95 | | 2.95 | | 2.95 | | 2.95 | | 2.94 | | 2.95 | |
| Afgas H _c (MJ kg ⁻¹) | 0.00 | | 0.00 | | 0.00 | | 0.00 | | 0.01 | | 0.00 | | 0.00 | |

Tabel 7-11: Sintesegas samestelling en berekende opbrengste, 35 mm krummels

| Eksp 221102_1 | | | | | | | | | | | | | | | | | | | | |
|---|-------------|--------------|-------------|--------------|-------------|--------------|-------------|--------------|-------------|--------------|-------------|--------------|-------------|--------------|-------------|--------------|-------------|--------------|-------------|--------------|
| Analises | 1 | | 2 | | 3 | | 4 | | 5 | | 6 | | 7 | | 8 | | 9 | | 10 | |
| Tyd | 10:15:00 | | 10:20:00 | | 10:25:00 | | 10:30:00 | | 10:35:00 | | 10:40:00 | | 10:45:00 | | 10:50:00 | | 10:55:00 | | 11:00:10 | |
| t = 0: voer begin | 0 | | 5 | | 10 | | 15 | | 20 | | 25 | | 30 | | 35 | | 40 | | 45 | |
| Samestelling | Mol | % m/m | Mol | % m/m | Mol | % m/m | Mol | % m/m | Mol | % m/m | Mol | % m/m | Mol | % m/m | Mol | % m/m | Mol | % m/m | Mol | % m/m |
| Totale C | 0.00 | 0.12% | 0.00 | 0.10% | 0.00 | 0.03% | 0.00 | 0.10% | 0.00 | 0.05% | 0.00 | 0.06% | 0.00 | 0.04% | 0.00 | 0.06% | 0.00 | 0.07% | 0.00 | 0.10% |
| Totale H | 0.00 | 0.00% | 0.00 | 0.00% | 0.00 | 0.00% | 0.00 | 0.00% | 0.00 | 0.00% | 0.00 | 0.00% | 0.00 | 0.00% | 0.00 | 0.00% | 0.00 | 0.00% | 0.00 | 0.01% |
| Totale O | 0.01 | 0.32% | 0.01 | 0.27% | 0.00 | 0.08% | 0.01 | 0.28% | 0.00 | 0.14% | 0.00 | 0.15% | 0.00 | 0.12% | 0.00 | 0.16% | 0.00 | 0.19% | 0.00 | 0.25% |
| Totale N | 1.59 | 73.39% | 1.60 | 74.05% | 1.61 | 74.46% | 1.61 | 74.43% | 1.61 | 74.57% | 1.60 | 73.95% | 1.61 | 74.62% | 1.61 | 74.53% | 1.59 | 73.84% | 1.60 | 74.23% |
| Totale Ar | 0.20 | 26.16% | 0.19 | 25.58% | 0.19 | 25.42% | 0.19 | 25.18% | 0.19 | 25.23% | 0.20 | 25.84% | 0.19 | 25.22% | 0.19 | 25.25% | 0.20 | 25.90% | 0.19 | 25.40% |
| Totaal | 100% | | 100% | | 100% | | 100% | | 100% | | 100% | | 100% | | 100% | | 100% | | 100% | |
| N ₂ + Ar (kg/h) | 2.93 | | 2.93 | | 2.93 | | 2.93 | | 2.93 | | 2.93 | | 2.93 | | 2.93 | | 2.93 | | 2.93 | |
| Singas (kg/h) | 0.0131 | | 0.0110 | | 0.0034 | | 0.0113 | | 0.0057 | | 0.0062 | | 0.0047 | | 0.0066 | | 0.0077 | | 0.0108 | |
| Afgas (kg/h) | 2.95 | | 2.95 | | 2.94 | | 2.95 | | 2.94 | | 2.94 | | 2.94 | | 2.94 | | 2.94 | | 2.95 | |
| Afgas H _c (MJ kg ⁻¹) | 0.00 | | 0.00 | | 0.00 | | 0.00 | | 0.00 | | 0.00 | | 0.00 | | 0.00 | | | | | |

Tabel 7-12: Sintesegas samestelling en berekende opbrengste, 35 mm krummels

| Eksp 221123_1 | | | | | | | | | | |
|---|------------|--------------|------------|--------------|------------|--------------|------------|--------------|------------|--------------|
| Analises | 1 | | 2 | | 3 | | 4 | | 5 | |
| t = 0: voer begin | 09:46:00 | | 09:57:00 | | 10:07:00 | | 10:17:00 | | 10:27:00 | |
| Looptyd (min) | 4 | | 15 | | 25 | | 35 | | 45. | |
| Samestelling | Mol | % m/m | Mol | % m/m | Mol | % m/m | Mol | % m/m | Mol | % m/m |
| Totale C | 0.40 | 20.86% | 0.37 | 16.92% | 0.42 | 22.74% | 0.00 | 0.05% | 0.39 | 22.11% |
| Totale H | 0.83 | 3.60% | 0.34 | 1.30% | 0.94 | 4.25% | 0.00 | 0.00% | 0.83 | 3.90% |
| Totale O | 0.33 | 22.38% | 0.39 | 23.58% | 0.33 | 23.28% | 0.00 | 0.14% | 0.31 | 23.36% |
| Totale N | 0.78 | 46.79% | 0.93 | 49.58% | 0.68 | 42.77% | 1.61 | 74.60% | 0.68 | 44.30% |
| Totale Ar | 0.04 | 6.36% | 0.06 | 8.63% | 0.04 | 6.95% | 0.19 | 25.21% | 0.03 | 6.34% |
| Totaal | 100% | | 100% | | 100% | | 100% | | 100% | |
| N ₂ + Ar (kg/h) | 2.93 | | 2.93 | | 2.93 | | 2.93 | | 2.93 | |
| Singas (kg/h) | 2.59 | | 2.11 | | 2.97 | | 0.01 | | 2.86 | |
| Afgas (kg/h) | 5.52 | | 5.04 | | 5.90 | | 2.94 | | 5.80 | |
| Afgas H _c (MJ kg ⁻¹) | -8.36 | | -4.70 | | -9.85 | | -3.65 | | -9.07 | |

Tabel 7-13: Opsomming van afgassamestelling en opbrengs, piroliseproses

| Eksp 221020 | | | | | | | | | | | | | | |
|----------------------------|----------|--------|----------|--------|----------|--------|----------|--------|----------|--------|----------|--------|----------|--------|
| Analises | 1 | | 2 | | 3 | | 4 | | 5 | | 6 | | 7 | |
| t = 0: plasma aan | 10:32:00 | | 10:41:20 | | 10:55:10 | | 11:04:00 | | 11:17:00 | | 11:25:50 | | 11:38:00 | |
| Looptyd (min) | 26 | | 35 | | 49 | | 58 | | 71 | | 80 | | 85 | |
| Samestelling | Mol | % m/m | Mol | % m/m | Mol | % m/m | Mol | % m/m | Mol | % m/m | Mol | % m/m | Mol | % m/m |
| Totale C | 0.00 | 0.05% | 0.00 | 0.12% | 0.00 | 0.15% | 0.00 | 0.11% | 0.00 | 0.15% | 0.00 | 0.02% | 0.00 | 0.14% |
| Totale H | 0.00 | 0.00% | 0.00 | 0.00% | 0.00 | 0.00% | 0.00 | 0.00% | 0.00 | 0.01% | 0.00 | 0.00% | 0.00 | 0.00% |
| Totale O | 0.00 | 0.14% | 0.01 | 0.31% | 0.01 | 0.39% | 0.01 | 0.29% | 0.01 | 0.41% | 0.00 | 0.05% | 0.01 | 0.38% |
| Totale N ₂ | 1.63 | 75.70% | 1.63 | 75.85% | 1.63 | 75.84% | 1.64 | 76.12% | 1.64 | 76.19% | 1.63 | 75.82% | 1.64 | 77.15% |
| Totale Ar | 0.18 | 24.11% | 0.18 | 23.73% | 0.18 | 23.62% | 0.18 | 23.49% | 0.18 | 23.24% | 0.18 | 24.11% | 0.17 | 22.33% |
| Totaal | 100.00% | | 100.00% | | 100.00% | | 100.00% | | 100.00% | | 100.00% | | 100.00% | |
| N ₂ + Ar (kg/h) | 2.93 | | 2.93 | | 2.93 | | 2.93 | | 2.93 | | 2.93 | | 2.93 | |
| Singas (kg/h) | 0.0057 | | 0.0125 | | 0.0160 | | 0.0118 | | 0.0168 | | 0.0021 | | 0.0153 | |
| Afgas (kg/h) | 2.94 | | 2.95 | | 2.95 | | 2.95 | | 2.95 | | 2.94 | | 2.95 | |

Tabel 7-14: Samestelling en singasopbrengs, tru- Boudouard proses

| Eksp 221102 | | | | | | | | | | | | | | | | | | | | |
|-------------------|----------|--------|----------|--------|----------|--------|----------|--------|----------|--------|----------|--------|----------|--------|----------|--------|----------|--------|----------|--------|
| Analises | 1 | | 2 | | 3 | | 4 | | 5 | | 6 | | 7 | | 8 | | 9 | | 10 | |
| Tyd | 10:15:00 | | 10:20:00 | | 10:25:00 | | 10:30:00 | | 10:35:00 | | 10:40:00 | | 10:45:00 | | 10:50:00 | | 10:55:00 | | 11:00:10 | |
| t = 0: voer begin | 0 | | 5 | | 10 | | 15 | | 20 | | 25 | | 30 | | 35 | | 40 | | 45 | |
| Samestelling | Mol | % m/m | Mol | % m/m | Mol | % m/m | Mol | % m/m | Mol | % m/m | Mol | % m/m | Mol | % m/m | Mol | % m/m | Mol | % m/m | Mol | % m/m |
| Totale C | 0.00 | 0.12% | 0.00 | 0.10% | 0.00 | 0.03% | 0.00 | 0.10% | 0.00 | 0.05% | 0.00 | 0.06% | 0.00 | 0.04% | 0.00 | 0.06% | 0.00 | 0.07% | 0.00 | 0.10% |
| Totale H | 0.00 | 0.00% | 0.00 | 0.00% | 0.00 | 0.00% | 0.00 | 0.00% | 0.00 | 0.00% | 0.00 | 0.00% | 0.00 | 0.00% | 0.00 | 0.00% | 0.00 | 0.00% | 0.00 | 0.01% |
| Totale O | 0.01 | 0.32% | 0.01 | 0.27% | 0.00 | 0.08% | 0.01 | 0.28% | 0.00 | 0.14% | 0.00 | 0.15% | 0.00 | 0.12% | 0.00 | 0.16% | 0.00 | 0.19% | 0.00 | 0.25% |
| Totale N | 1.59 | 73.39% | 1.60 | 74.05% | 1.61 | 74.46% | 1.61 | 74.43% | 1.61 | 74.57% | 1.60 | 73.95% | 1.61 | 74.62% | 1.61 | 74.53% | 1.59 | 73.84% | 1.60 | 74.23% |
| Totale Ar | 0.20 | 26.16% | 0.19 | 25.58% | 0.19 | 25.42% | 0.19 | 25.18% | 0.19 | 25.23% | 0.20 | 25.84% | 0.19 | 25.22% | 0.19 | 25.25% | 0.20 | 25.90% | 0.19 | 25.40% |
| Totaal | 100% | | 100% | | 100% | | 100% | | 100% | | 100% | | 100% | | 100% | | 100% | | 100% | |
| N2 + Ar (kg/h) | 2.93 | | 2.93 | | 2.93 | | 2.93 | | 2.93 | | 2.93 | | 2.93 | | 2.93 | | 2.93 | | 2.93 | |
| Singas (kg/h) | 0.0131 | | 0.0110 | | 0.0034 | | 0.0113 | | 0.0057 | | 0.0062 | | 0.0047 | | 0.0066 | | 0.0077 | | 0.0108 | |
| Afgas (kg/h) | 2.95 | | 2.95 | | 2.94 | | 2.95 | | 2.94 | | 2.94 | | 2.94 | | 2.94 | | 2.94 | | 2.95 | |
| Eksp 221123_1 | | | | | | | | | | | | | | | | | | | | |
| Analises | 1 | | 2 | | 3 | | 4 | | 5 | | | | | | | | | | | |
| t = 0: voer begin | 09:46:00 | | 09:57:00 | | 10:07:00 | | 10:17:00 | | 10:27:00 | | | | | | | | | | | |
| Looptyd (min) | 4 | | 15 | | 25 | | 35 | | 45. | | | | | | | | | | | |
| Samestelling | Mol | % m/m | Mol | % m/m | Mol | % m/m | Mol | % m/m | Mol | % m/m | | | | | | | | | | |
| Totale C | 0.40 | 20.86% | 0.37 | 16.92% | 0.42 | 22.74% | 0.00 | 0.05% | 0.39 | 22.11% | | | | | | | | | | |

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